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## Double Conjugate Addition of Dithiols to Propargylic Carbonyl Systems To Generate Protected 1,3-Dicarbonyl Compounds

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multi-scan from symmetry-related measurements
Sortav (Blessing 1995)
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The absolute structure was determined (Flack parameter 0.05(7)).
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on F, with F set to zero for negative F2. The threshold expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
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O3 O 0.6917(2) 0.4743(3) -0.12513(12) 0.0413(5) Uani 1 1 d . . .
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H2B H 0.4101 0.3802 0.1280 0.042 Uiso 1 1 calc R . .
H2C H 0.2496 0.2408 0.1225 0.042 Uiso 1 1 calc R . .
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H4B H 0.4661 0.6056 0.0364 0.040 Uiso 1 1 calc R . .
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H6B H 0.3389 0.0355 -0.0533 0.079 Uiso 1 1 calc R . .
H6C H 0.3247 0.1338 -0.1226 0.079 Uiso 1 1 calc R . .
C7 C 0.0391(5) 0.4550(6) 0.0361(3) 0.0696(12) Uani 1 1 d . . .
H7A H 0.0892 0.5327 -0.0051 0.084 Uiso 1 1 calc R . .
H7B H -0.0677 0.4140 0.0299 0.084 Uiso 1 1 calc R . .
C8 C 0.0855(5) 0.5190(5) 0.1195(3) 0.0638(10) Uani 1 1 d . . .
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H8B H 0.1093 0.6224 0.1190 0.077 Uiso 1 1 calc R . .

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C9 C 0.3238(4) 0.4141(4) -0.13708(17) 0.0387(6) Uani 1 1 d . . .
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H9B H 0.2773 0.4744 -0.1461 0.046 Uiso 1 1 calc R . .
C10 C 0.3918(4) 0.4039(4) -0.21671(19) 0.0488(8) Uani 1 1 d . . .
H10 H 0.4522 0.3572 -0.2053 0.059 Uiso 1 1 calc R . .
C11 C 0.2720(5) 0.3070(5) -0.2768(2) 0.0662(12) Uani 1 1 d . . .
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H11B H 0.2046 0.3447 -0.2840 0.099 Uiso 1 1 calc R . .
H11C H 0.2181 0.2068 -0.2558 0.099 Uiso 1 1 calc R . .
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H12B H 0.5732 0.6091 -0.2163 0.094 Uiso 1 1 calc R . .
H12C H 0.4351 0.6041 -0.2597 0.094 Uiso 1 1 calc R . .
C13 C 0.7515(3) 0.5566(3) 0.02371(15) 0.0297(5) Uani 1 1 d . . .
C14 C 0.7385(3) 0.5275(3) 0.10620(16) 0.0324(6) Uani 1 1 d . . .
H14 H 0.6728 0.4320 0.1258 0.039 Uiso 1 1 calc R . .
C15 C 0.8224(3) 0.6394(3) 0.15964(16) 0.0363(6) Uani 1 1 d . . .
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C16 C 0.9202(3) 0.7800(3) 0.13252(17) 0.0373(6) Uani 1 1 d . . .
C17 C 0.9327(4) 0.8048(3) 0.04942(18) 0.0426(7) Uani 1 1 d . . .
H17 H 1.0004 0.8996 0.0297 0.051 Uiso 1 1 calc R . .
C18 C 0.8495(4) 0.6958(3) -0.00499(16) 0.0393(7) Uani 1 1 d . . .
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C19 C 1.0135(5) 0.9002(4) 0.1910(2) 0.0558(9) Uani 1 1 d . . .
H19A H 0.9517 0.9052 0.2339 0.084 Uiso 1 1 calc R . .
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C3 0.0258(13) 0.0306(14) 0.0439(14) -0.0053(11) 0.0014(11) 0.0148(12)
C4 0.0336(15) 0.0280(14) 0.0421(14) -0.0025(11) 0.0005(11) 0.0173(12)
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C6 0.057(2) 0.0410(19) 0.067(2) -0.0191(16) -0.0157(17) 0.0291(17)
C7 0.058(2) 0.085(3) 0.091(3) -0.001(2) 0.000(2) 0.055(3)
C8 0.059(2) 0.062(2) 0.088(3) 0.003(2) 0.017(2) 0.044(2)
C9 0.0403(16) 0.0446(17) 0.0415(14) -0.0037(13) -0.0072(12) 0.0290(15)
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C17 0.0446(18) 0.0318(15) 0.0422(15) 0.0077(12) 0.0033(13) 0.0123(14)
C18 0.0466(17) 0.0388(16) 0.0302(12) 0.0071(11) 0.0048(12) 0.0196(14)
C19 0.060(2) 0.0432(19) 0.0474(16) -0.0056(14) -0.0060(15) 0.0130(17)

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are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

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S3 O3 1.434(2) . ?
S3 O2 1.436(2) . ?
S3 N1 1.630(2) . ?
S3 C13 1.770(3) . ?
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O1 C6 1.431(4) . ?
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C12 C10 C11 110.6(3) . . ?  
C9 C10 C11 110.1(3) . . ?  
C12 C10 H10 108.1 . . ?  
C9 C10 H10 108.1 . . ?  
C11 C10 H10 108.1 . . ?  
C10 C11 H11A 109.5 . . ?  
C10 C11 H11B 109.5 . . ?  
H11A C11 H11B 109.5 . . ?  
C10 C11 H11C 109.5 . . ?  
H11A C11 H11C 109.5 . . ?  
H11B C11 H11C 109.5 . . ?  
C10 C12 H12A 109.5 . . ?  
C10 C12 H12B 109.5 . . ?  
H12A C12 H12B 109.5 . . ?  
C10 C12 H12C 109.5 . . ?  
H12A C12 H12C 109.5 . . ?  
H12B C12 H12C 109.5 . . ?  
C14 C13 C18 120.5(3) . . ?  
C14 C13 S3 119.5(2) . . ?  
C18 C13 S3 120.0(2) . . ?  
C15 C14 C13 119.0(3) . . ?  
C15 C14 H14 120.5 . . ?  
C13 C14 H14 120.5 . . ?  
C14 C15 C16 121.6(3) . . ?  
C14 C15 H15 119.2 . . ?  
C16 C15 H15 119.2 . . ?  
C17 C16 C15 117.9(3) . . ?  
C17 C16 C19 120.9(3) . . ?  
C15 C16 C19 121.2(3) . . ?  
C18 C17 C16 121.7(3) . . ?  
C18 C17 H17 119.2 . . ?  
C16 C17 H17 119.2 . . ?  
C17 C18 C13 119.3(3) . . ?  
C17 C18 H18 120.4 . . ?  
C13 C18 H18 120.4 . . ?  
C16 C19 H19A 109.5 . . ?  
C16 C19 H19B 109.5 . . ?  
H19A C19 H19B 109.5 . . ?  
C16 C19 H19C 109.5 . . ?  
H19A C19 H19C 109.5 . . ?  
H19B C19 H19C 109.5 . . ?

loop\_

\_geom\_torsion\_atom\_site\_label\_1  
\_geom\_torsion\_atom\_site\_label\_2  
\_geom\_torsion\_atom\_site\_label\_3  
\_geom\_torsion\_atom\_site\_label\_4  
\_geom\_torsion  
\_geom\_torsion\_site\_symmetry\_1  
\_geom\_torsion\_site\_symmetry\_2  
\_geom\_torsion\_site\_symmetry\_3  
\_geom\_torsion\_site\_symmetry\_4



\_geom\_torsion\_publ\_flag

O3 S3 N1 C1 155.1(2) . . . . ?  
O2 S3 N1 C1 25.4(2) . . . . ?  
C13 S3 N1 C1 -90.6(2) . . . . ?  
O3 S3 N1 C5 -41.6(2) . . . . ?  
O2 S3 N1 C5 -171.3(2) . . . . ?  
C13 S3 N1 C5 72.7(2) . . . . ?  
C6 O1 C1 N1 63.6(3) . . . . ?  
C6 O1 C1 C2 -174.3(3) . . . . ?  
C5 N1 C1 O1 72.0(3) . . . . ?  
S3 N1 C1 O1 -124.7(2) . . . . ?  
C5 N1 C1 C2 -46.8(3) . . . . ?  
S3 N1 C1 C2 116.5(2) . . . . ?  
O1 C1 C2 C3 -72.6(3) . . . . ?  
N1 C1 C2 C3 48.9(3) . . . . ?  
C1 C2 C3 C4 -51.4(3) . . . . ?  
C1 C2 C3 S2 76.1(3) . . . . ?  
C1 C2 C3 S1 -170.3(2) . . . . ?  
C7 S2 C3 C2 157.7(2) . . . . ?  
C7 S2 C3 C4 -77.9(3) . . . . ?  
C7 S2 C3 S1 42.2(2) . . . . ?  
C8 S1 C3 C2 -147.0(2) . . . . ?  
C8 S1 C3 C4 94.8(2) . . . . ?  
C8 S1 C3 S2 -28.6(2) . . . . ?  
C2 C3 C4 C5 52.4(3) . . . . ?  
S2 C3 C4 C5 -73.3(3) . . . . ?  
S1 C3 C4 C5 169.7(2) . . . . ?  
C1 N1 C5 C9 -82.9(3) . . . . ?  
S3 N1 C5 C9 113.5(2) . . . . ?  
C1 N1 C5 C4 46.3(3) . . . . ?  
S3 N1 C5 C4 -117.3(2) . . . . ?  
C3 C4 C5 N1 -49.2(3) . . . . ?  
C3 C4 C5 C9 77.8(3) . . . . ?  
C3 S2 C7 C8 -45.6(3) . . . . ?  
S2 C7 C8 S1 30.1(4) . . . . ?  
C3 S1 C8 C7 0.0(3) . . . . ?  
N1 C5 C9 C10 -73.3(3) . . . . ?  
C4 C5 C9 C10 160.6(3) . . . . ?  
C5 C9 C10 C12 -69.7(3) . . . . ?  
C5 C9 C10 C11 167.1(3) . . . . ?  
O3 S3 C13 C14 -174.9(2) . . . . ?  
O2 S3 C13 C14 -45.5(2) . . . . ?  
N1 S3 C13 C14 69.7(2) . . . . ?  
O3 S3 C13 C18 4.0(3) . . . . ?  
O2 S3 C13 C18 133.4(2) . . . . ?  
N1 S3 C13 C18 -111.3(2) . . . . ?  
C18 C13 C14 C15 1.1(4) . . . . ?  
S3 C13 C14 C15 -180.0(2) . . . . ?  
C13 C14 C15 C16 -0.4(4) . . . . ?  
C14 C15 C16 C17 -0.8(5) . . . . ?  
C14 C15 C16 C19 -178.6(3) . . . . ?  
C15 C16 C17 C18 1.4(5) . . . . ?  
C19 C16 C17 C18 179.2(3) . . . . ?  
C16 C17 C18 C13 -0.8(5) . . . . ?  
C14 C13 C18 C17 -0.5(4) . . . . ?  
S3 C13 C18 C17 -179.4(3) . . . . ?

_diffraction_measured_fraction_theta_max	0.997
_diffraction_reflns_theta_full	27.48
_diffraction_measured_fraction_theta_full	0.997
_refine_diff_density_max	0.423
_refine_diff_density_min	-0.224
_refine_diff_density_rms	0.053